

# Continuity equation

$$R.T.T.: \frac{DB_{sys}}{Dt} = \frac{DB_{cv}}{Dt} + \int_{CS} \rho b \vec{V} \cdot \vec{n} dA$$

Let  $B_{sys} = M_{sys}$  the mass of the system

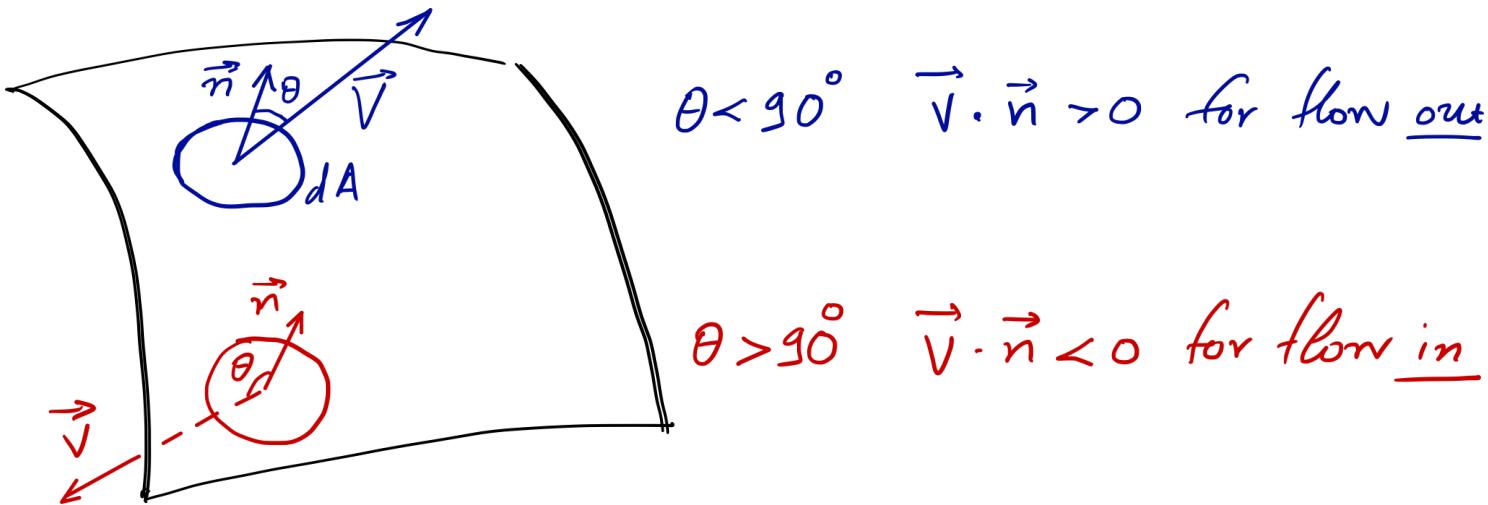
then  $b = 1$

Conservation of mass principle:  $\frac{DM_{sys}}{Dt} = 0$

Hence:  $\frac{\partial M_{cv}}{\partial t} + \int_{CS} \rho \vec{V} \cdot \vec{n} dA = 0$

or 
$$\underbrace{\frac{\partial}{\partial t} \int_{cv} \rho dV}_{\text{time rate of change of mass inside the C.V.}} + \underbrace{\int_{CS} \rho \vec{V} \cdot \vec{n} dA}_{\text{net rate of flow of mass through the control surface}} = 0$$

# Conservation of mass



$$\int_{CS} \underbrace{\vec{V} \cdot \vec{n} dA}_{\substack{\text{flowrate} \\ \text{through } dA}} = \mathcal{I}_{\text{inout}} - \sum \mathcal{I}_{\text{in}}$$

$\underbrace{\quad}_{\substack{\text{mass flowrate} \\ \text{through } dA}}$

Rewrite as

$$\frac{\partial}{\partial t} \int_{cv} e dt + \Sigma \dot{m}_{out} - \Sigma \dot{m}_{in} = 0$$

For steady flows  $\frac{\partial}{\partial t} (\quad) = 0$

$$\text{So, } \Sigma \dot{m}_{out} - \Sigma \dot{m}_{in} = 0$$

$$\text{or } \Sigma \dot{m}_{out} = \Sigma \dot{m}_{in}$$

The mass flowrate,  $\dot{m}$ , is also given as

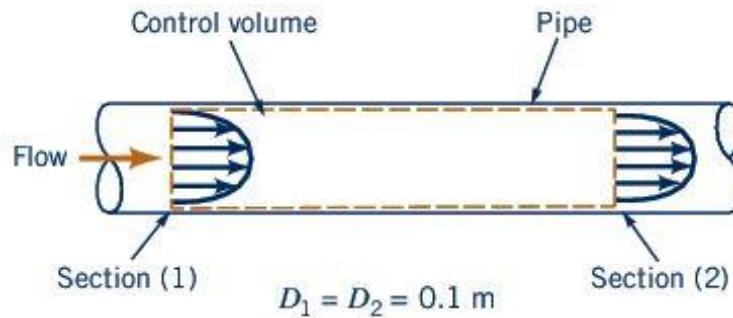
$$\dot{m} = \rho \cdot Q = \rho \cdot \underbrace{V \cdot A}_{\substack{\uparrow \text{density} \quad \uparrow \text{flowrate}}} \quad \text{only when } V \text{ is } \underline{\text{constant}} \text{ across } A \text{ and } \underline{\text{perpendicular to area } A}$$

If  $V$  is not uniform, use the average velocity  $\bar{V}$

$$\bar{V} = \frac{\int_A e \vec{V} \cdot \vec{n} dA}{eA}$$

$$\dot{m} = \rho \bar{V} \cdot A$$

# Example 1: Continuity in compressible fluid flow



$$p_1 = 690 \text{ kPa}$$
$$T_1 = 27^\circ\text{C}$$

$$p_2 = 127 \text{ kPa}$$
$$T_2 = -21^\circ\text{C}$$
$$\bar{V}_2 = 305 \text{ m/s}$$

Continuity:  $\frac{\partial}{\partial t} \int_{CV} \rho dt + \dot{m}_{out} - \dot{m}_{in} = 0$

$\Rightarrow 0 \text{ (steady flow)}$

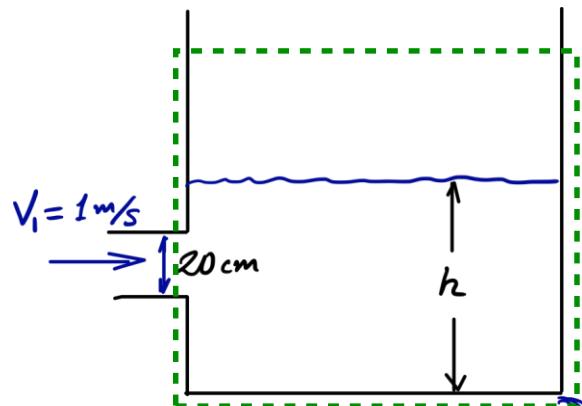
$$\Rightarrow \dot{m}_{out} = \dot{m}_{in} \Rightarrow \rho_1 \bar{V}_1 A_1 = \rho_2 \bar{V}_2 A_2$$

and since  $A_1 = A_2$ :  $\rho_1 \bar{V}_1 = \rho_2 \bar{V}_2 \Rightarrow \bar{V}_1 = \frac{\rho_2}{\rho_1} \bar{V}_2$

From ideal gas law:  $\rho = \frac{P}{RT}$

Hence,  $\bar{V}_1 = \frac{P_2 T_1 \bar{V}_2}{P_1 T_2} = \frac{127 \text{ kPa}}{690 \text{ kPa}} \cdot \frac{300 \text{ K}}{252 \text{ K}} \cdot 305 \text{ m/s} \Rightarrow \underline{\underline{\bar{V}_1 = 66.8 \text{ m/s}}}$

## Example 2: continuity in unsteady flow



Rectangular container  
 $0.6 \text{ m} \times 0.6 \text{ m}$

Calculate:

- 1) How fast the water level rises?
- 2) How long does it take to rise 0.5 m?

leakage  $Q = 20 \text{ lit/min}$

Continuity:  $\frac{\partial}{\partial t} \int \rho dV + \sum m_{out} - \sum m_{in} = 0 \quad \rho = ct$

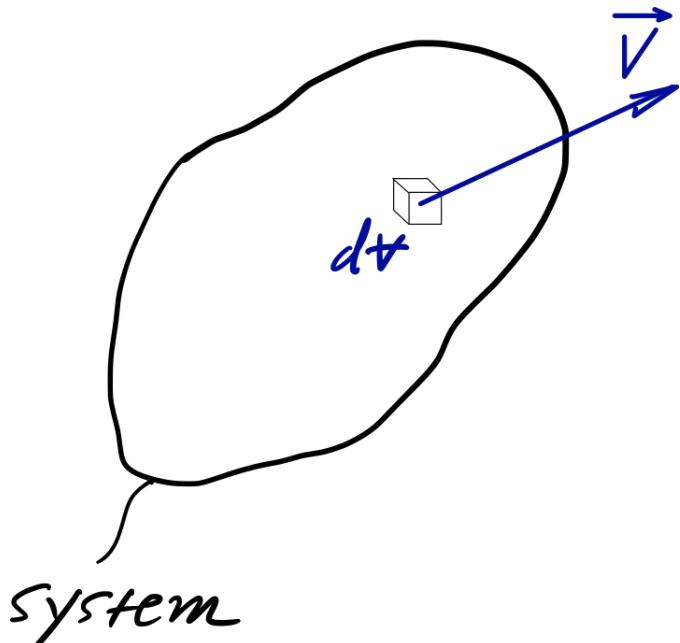
~~$\rho \frac{\partial}{\partial t} \int_{cv} dV + \rho \frac{cv}{Q_{out}} - \rho V_i A_i = 0$~~

$$\Rightarrow \frac{\partial}{\partial t} (0.6 \times 0.6 \times h) + 20 \text{ lit/min} \cdot \frac{10^{-3} \text{ m}^3/\text{lit}}{60 \text{ s/min}} - 1 \text{ m/s} \times \pi 0.1^2 \text{ m}^2 = 0$$

$$\Rightarrow 0.36 \frac{dh}{dt} + 3.33 \times 10^{-4} - 0.0314 = 0 \Rightarrow \frac{dh}{dt} = 0.0311 \text{ m/s}$$

$$t = \frac{\Delta h}{dh/dt} = \frac{0.5 \text{ m}}{0.0311 \text{ m/s}} = \underline{\underline{16.1 \text{ s}}}$$

# Linear momentum equation



system

Newton's 2<sup>nd</sup> law:

$$\frac{D}{Dt} \int_{sys} \vec{V} \cdot \rho dV = \sum \vec{F}_{sys}$$

$\underbrace{\int_{sys} \rho dV}_{dm}$   
 $\underbrace{\vec{V}}$  momentum  
in  $dV$

Apply the RTT ( $B = m\vec{V} \Rightarrow b = \vec{V}$ ):

$$\frac{\partial}{\partial t} \int_{cv} \vec{V} \rho dV + \int_{cs} \vec{V} \rho \vec{V} \cdot \vec{n} dA = \sum \vec{F}_{cv}$$

Sum of  
body and  
surface forces  
acting on the  
control volume

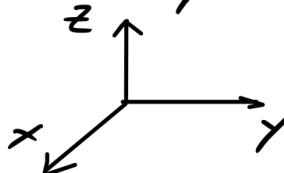
Linear momentum equation

# Linear momentum in x, y & z

When the flow is steady ( $\frac{\partial}{\partial t}(\cdot) = 0$ ):

$$\int_{CS} \vec{V} \rho \underbrace{\vec{V} \cdot \vec{n}}_{\text{scalar}} dA = \sum \vec{F}_{CV}$$

Vector equation



$$\vec{V} = u \vec{i} + v \vec{j} + w \vec{k}$$

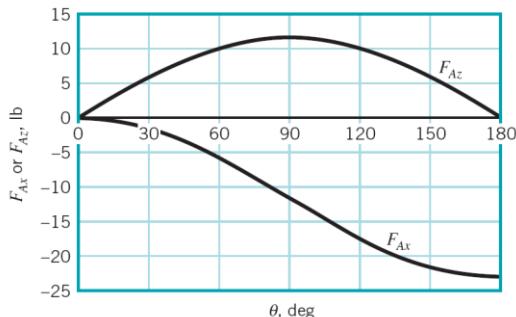
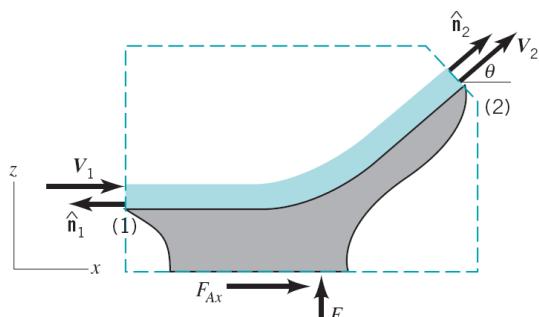
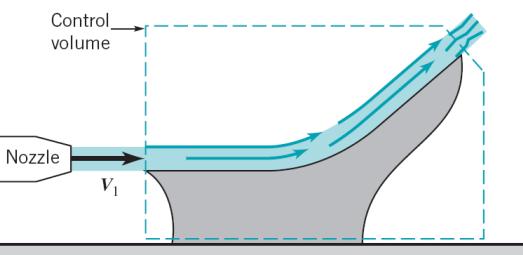
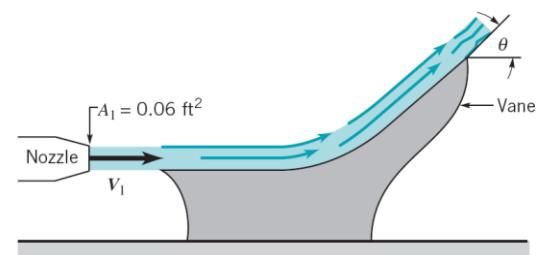
So, the linear momentum equation in x, y & z:

$$x: \int_{CS} u \rho \vec{V} \cdot \vec{n} dA = \sum F_x$$

$$y: \int_{CS} v \rho \vec{V} \cdot \vec{n} dA = \sum F_y$$

$$z: \int_{CS} w \rho \vec{V} \cdot \vec{n} dA = \sum F_z$$

# Example: linear momentum - change in flow direction



Linear momentum in  $x$  and  $z$  directions:

$$x: \cancel{\frac{\partial}{\partial t} \int_{cv} u \rho dt} + \int_{cs} u \rho \vec{v} \cdot \vec{n} dA = \sum F_x$$

$\cancel{cv}$   $\cancel{0 \text{ (steady)}}$

$$z: \cancel{\frac{\partial}{\partial t} \int_{cv} w \rho dt} + \int_{cs} w \rho \vec{v} \cdot \vec{n} dA = \sum F_z$$

$\cancel{cv}$   $\cancel{0 \text{ (steady)}}$

or  $V_1 \cdot \rho \cdot (-V_1) A_1 + (V_2 \cos \theta) \cdot \rho \cdot V_2 \cdot A_2 = F_{Ax}$

and  $0 + (V_2 \sin \theta) \cdot \rho \cdot V_2 \cdot A_2 = F_{Az}$

$P=0$   
(atm)  
No  
pressure  
forces

From continuity  $A_1 V_1 = A_2 V_2$ .

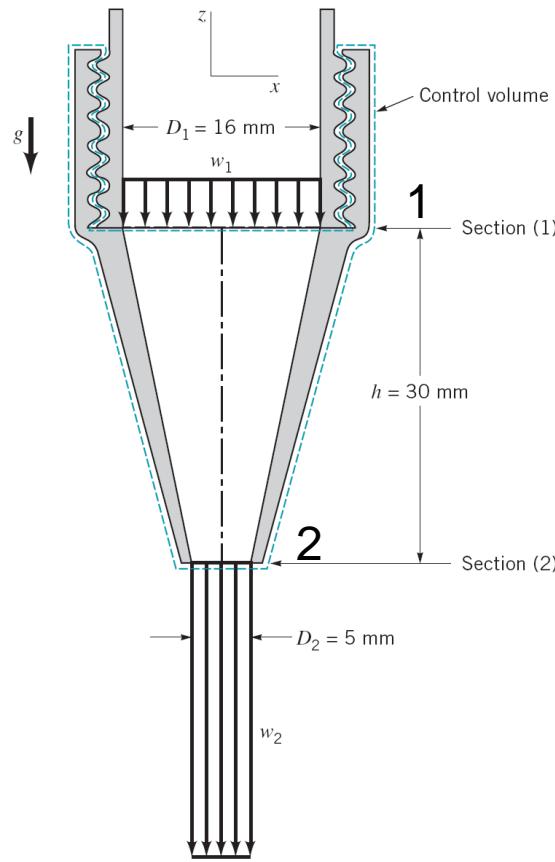
Bernoulli:  $\cancel{P_1} + \frac{1}{2} \rho V_1^2 + \gamma z_1 = \cancel{P_2} + \frac{1}{2} \rho V_2^2 + \gamma z_2$

since  $z_2 \approx z_1 \Rightarrow V_1 = V_2$

Hence:  $F_{Ax} = -\rho A_1 V_1^2 (1 - \cos \theta)$

and  $F_{Az} = \rho A_1 V_1^2 \sin \theta$

# Linear momentum: weight, pressure and speed change



What is the anchoring force to keep the nozzle in place?

From continuity:

$$Q = w_1 A_1 = w_2 A_2$$

$$w_1 = \frac{Q}{A_1} = \frac{0.6 \times 10^{-3} \text{ m}^3/\text{s}}{\pi \times 0.008^2 \text{ m}^2}$$

$$\underline{w_1 = 2.98 \text{ m/s}}$$

Flowrate:  $0.6 \text{ lit/s}$

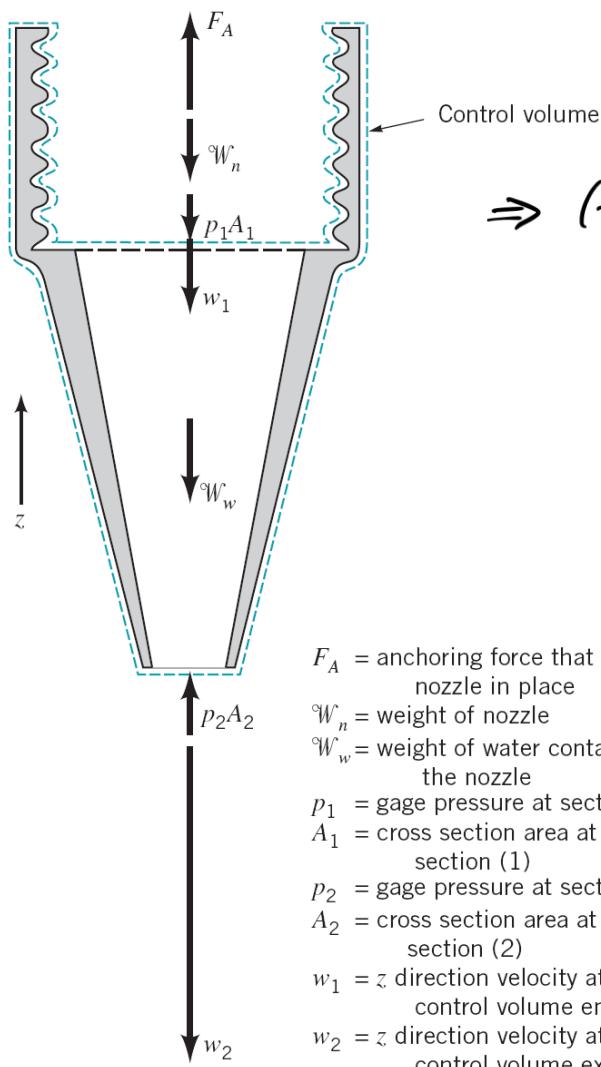
Nozzle mass:  $0.1 \text{ kg}$

$$P_1 = 464 \text{ kPa}$$

$$w_2 = \frac{A_1}{A_2} w_1 = \left(\frac{16}{5}\right)^2 2.98 \text{ m/s}$$

$$\underline{w_2 = 30.5 \text{ m/s}}$$

*z-momentum:*



$$\int_{CS} w \rho \vec{v} \cdot \vec{n} dA = F_A - W_n - P_1 A_1 - W_w + \cancel{P_2 A_2} \quad \text{O}$$

$$\Rightarrow (-w_1) \rho (-w_1) A_1 + (-w_2) \rho (w_2) A_2 = F_A - W_n - P_1 A_1 - W_w \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

Mass flowrate  $\dot{m} = \rho w_1 A_1 = \rho w_2 A_2$

$$\Rightarrow \dot{m} w_1 - \dot{m} w_2 = F_A - W_n - P_1 A_1 - W_w$$

$$\Rightarrow \underline{\underline{F_A = \dot{m} (w_1 - w_2) + P_1 A_1 + W_n + W_w}}$$

$F_A$  = anchoring force that holds nozzle in place

$W_n$  = weight of nozzle

$W_w$  = weight of water contained in the nozzle

$P_1$  = gage pressure at section (1)

$A_1$  = cross section area at section (1)

$P_2$  = gage pressure at section (2)

$A_2$  = cross section area at section (2)

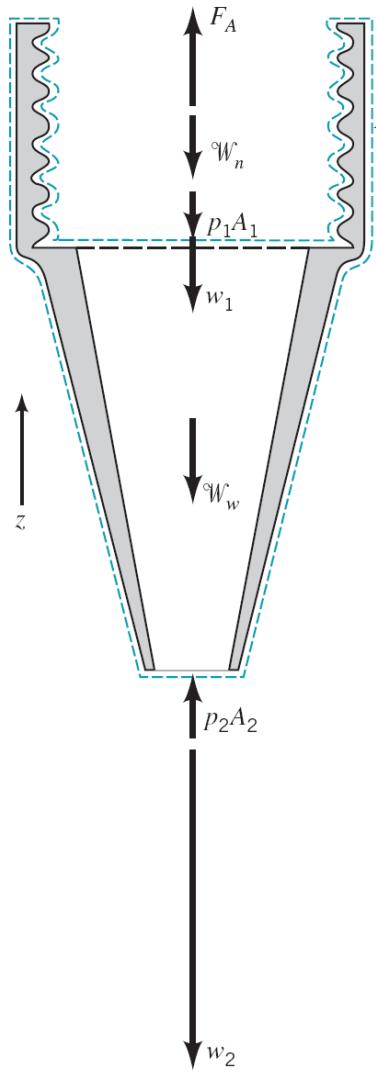
$w_1$  = z direction velocity at control volume entrance

$w_2$  = z direction velocity at control volume exit

$$\dot{m} = \rho \cdot Q = 999 \text{ kg/m}^3 \cdot 0.6 \text{ l/s} \cdot \frac{1 \text{ m}^3}{1000 \text{ l}} = 0.599 \text{ kg/s}$$

$$W_n = m_n \cdot g = 0.1 \text{ kg} \cdot 9.81 \text{ m/s}^2 = \underline{0.981 \text{ N}}$$

$$W_w = \rho \cdot V_w \cdot g$$



The volume of water,  $V_w$ , is calculated as the volume of the truncated cone:

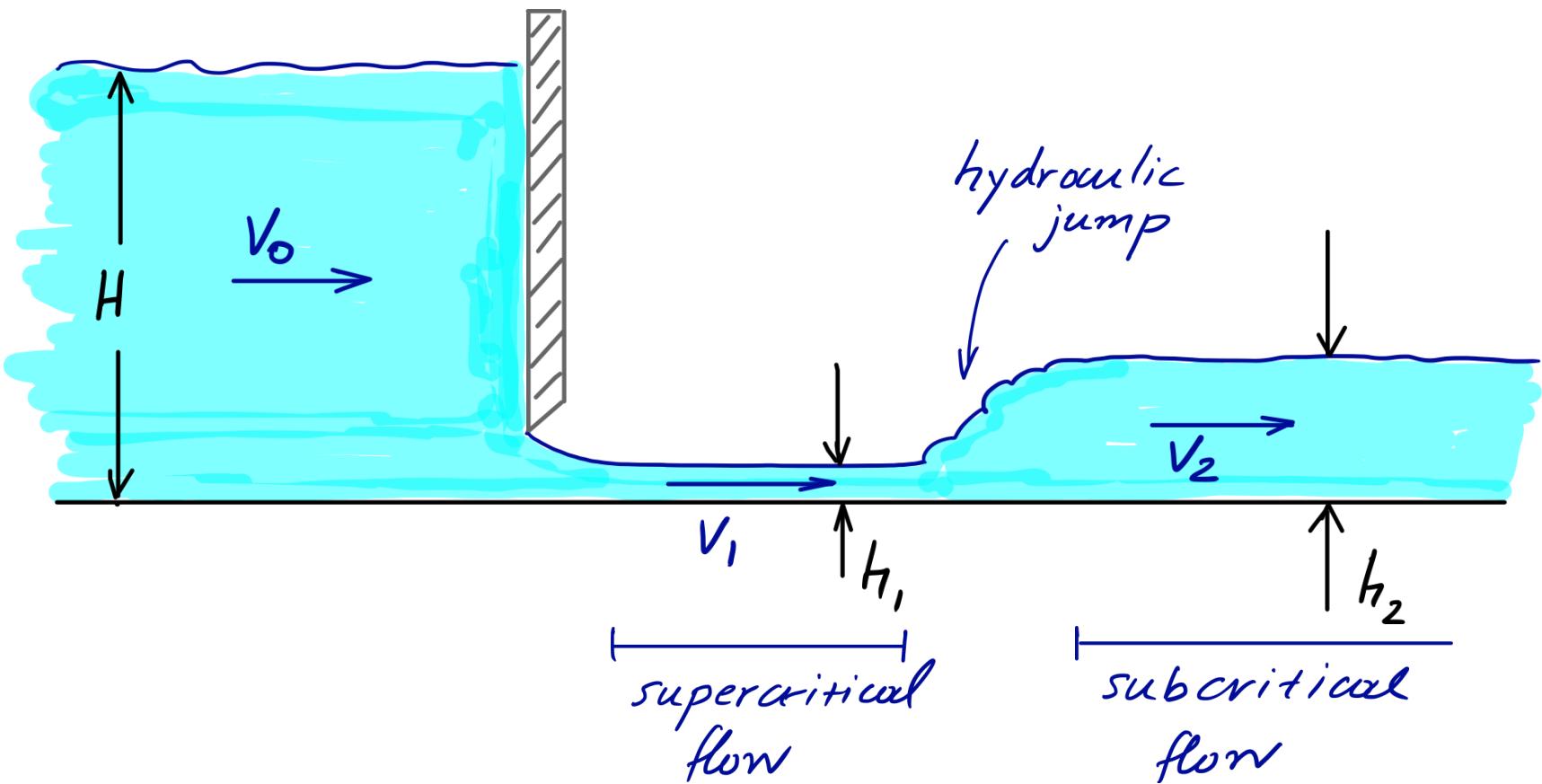
$$\begin{aligned} V_w &= \frac{1}{12} \pi h (R_1^2 + R_2^2 + R_1 R_2) \\ &= \frac{1}{12} \pi 0.03 (0.016^2 + 0.005^2 + 0.016 \times 0.005) \\ &= 2.84 \times 10^{-6} \text{ m}^3 \end{aligned}$$

$$\begin{aligned} \text{Hence, } W_w &= 999 \text{ kg/m}^3 \times 2.84 \times 10^{-6} \text{ m}^3 \times 9.81 \text{ m/s}^2 \\ &= \underline{0.0278 \text{ N}} \end{aligned}$$

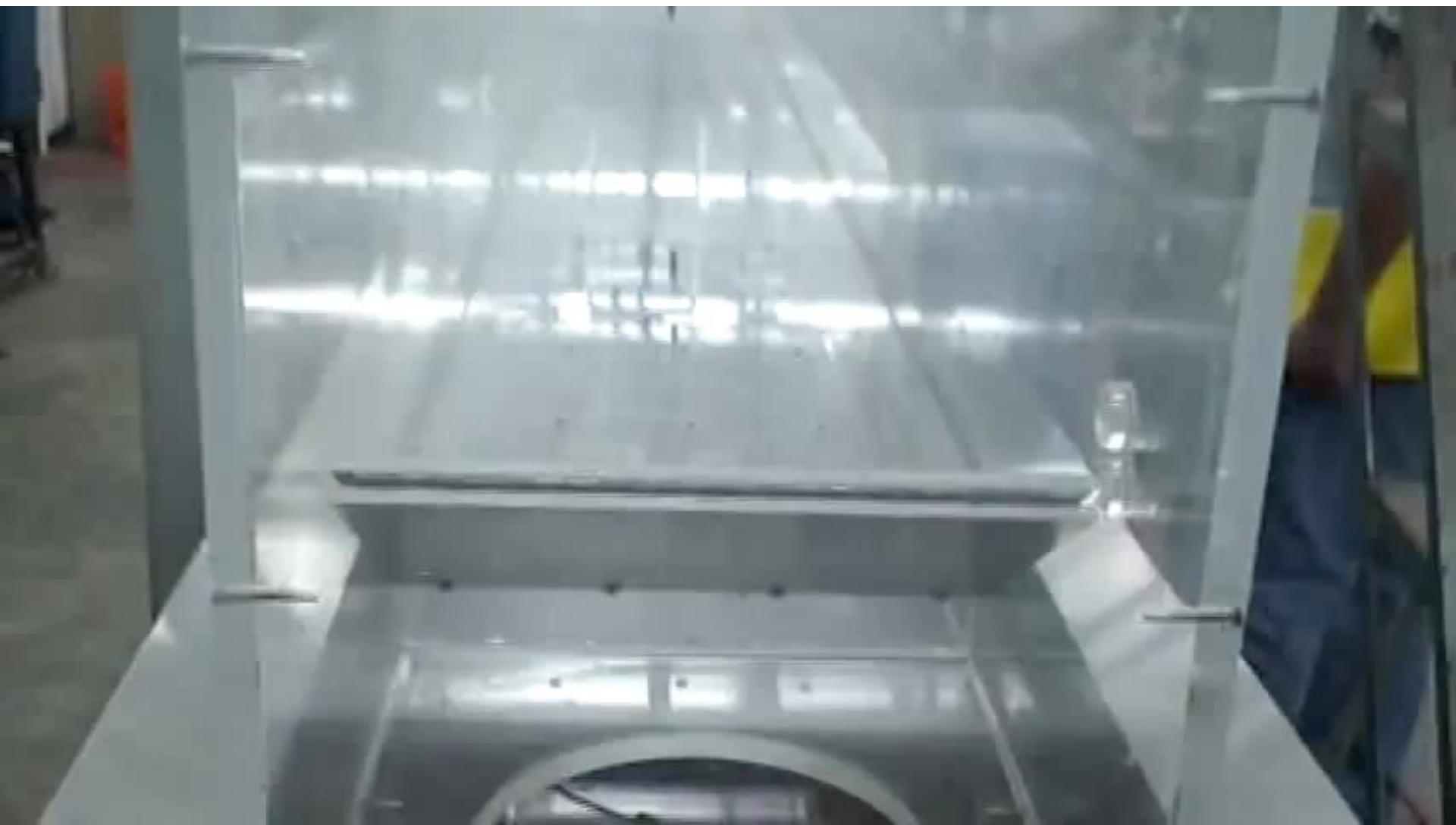
Finally, the anchoring force,  $F_A$ , is calculated as:

$$\begin{aligned} F_A &= m(W_n - W_w) + P_1 A_1 + W_n + W_w \\ &= 0.599 \text{ kg/s} (2.98 \text{ m/s} - 30.5 \text{ m/s}) + 464'000 \text{ N/m}^2 \times \pi 0.008^2 \text{ m}^2 \\ &\quad + 0.981 \text{ N} + 0.0278 \text{ N} \\ \Rightarrow F_A &= \underline{77.8 \text{ N}} \end{aligned}$$

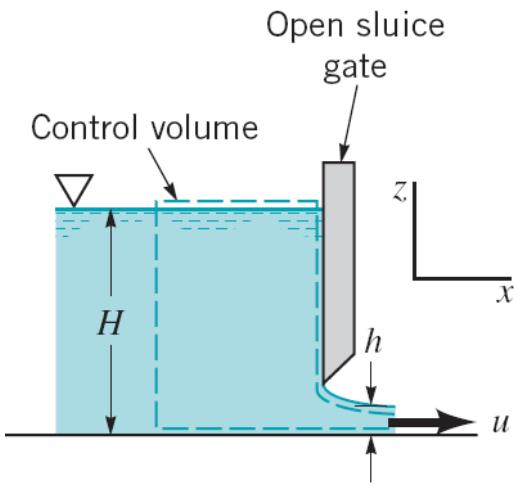
# Example: sluice gate



# Sluice gate hydraulic jump experiment (video)



# Part 1: force on sluice gate



Momentum (steady flow):

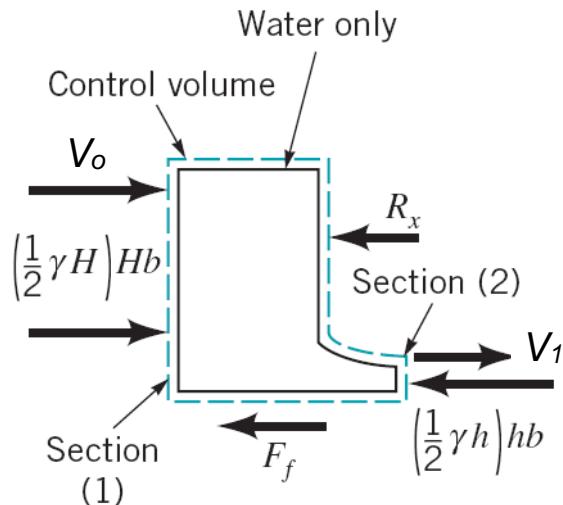
$$\int_{CS} u \rho \vec{V} \cdot \vec{n} dA = \Sigma F_x$$

$$\Rightarrow V_0 \rho (-V_0) A_0 + V_1 \rho V_1 A_1 = \gamma \frac{H}{2} (Hb) - \gamma \frac{h}{2} (h_b) - R_x$$

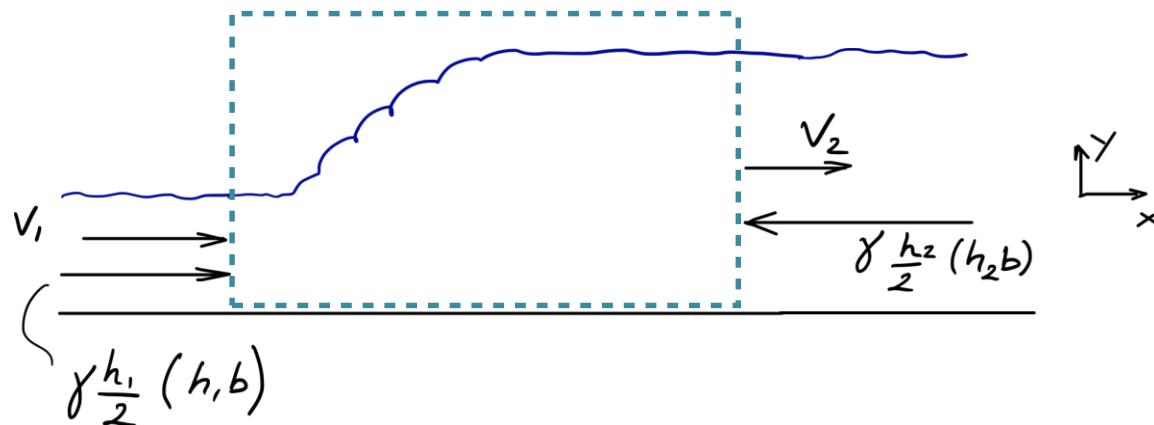
If  $h \ll H \rightarrow V_0 \ll V_1$ , then

$$R_x = \frac{1}{2} \gamma H^2 b - \rho V_1^2 b h_1$$

force on  
sluice gate  
when fully  
closed



## Part 2: height ratio across the hydraulic jump



$$\int_{CS} u \rho \vec{V} \cdot \vec{n} dA = \frac{1}{2} \gamma h_1^2 b - \frac{1}{2} \gamma h_2^2 b$$

$$\Rightarrow V_1 \rho (-V_1) A_1 + V_2 \rho (V_2) A_2 = \frac{1}{2} \gamma (h_1^2 - h_2^2) b$$

$$\Rightarrow -\rho V_1^2 h_1 b + \rho V_2^2 h_2 b = \frac{1}{2} \gamma (h_1^2 - h_2^2) b$$

Divide by  $\rho \cdot b$

$$\Rightarrow V_2^2 h_2 - V_1^2 h_1 = \frac{1}{2} g (h_1^2 - h_2^2) \quad (1)$$

From continuity,  $V_1 h_1 b = V_2 h_2 b \Rightarrow V_2 = V_1 \frac{h_1}{h_2}$

$$(1) \Rightarrow V_1^2 \frac{h_1^2}{h_2} - V_1^2 \cancel{h_1} = \frac{1}{2} g h_1 \cancel{h_1} \left( 1 - \frac{h_2^2}{h_1^2} \right)$$

$$\Rightarrow V_1^2 \left( \frac{h_1}{h_2} - 1 \right) = \frac{1}{2} g h_1 \left( 1 - \frac{h_2}{h_1} \right) \left( 1 + \frac{h_2}{h_1} \right)$$

$$\Rightarrow V_1^2 \frac{h_1}{h_2} \left( 1 - \frac{h_2}{h_1} \right) = \frac{1}{2} g h_1 \left( 1 - \frac{h_2}{h_1} \right) \left( 1 + \frac{h_2}{h_1} \right)$$

$$\Rightarrow \frac{V_1^2}{g h_1} = \frac{1}{2} \frac{h_2}{h_1} \left( 1 + \frac{h_2}{h_1} \right) \quad \text{let } F_r = \frac{V_1}{\sqrt{g h_1}}$$

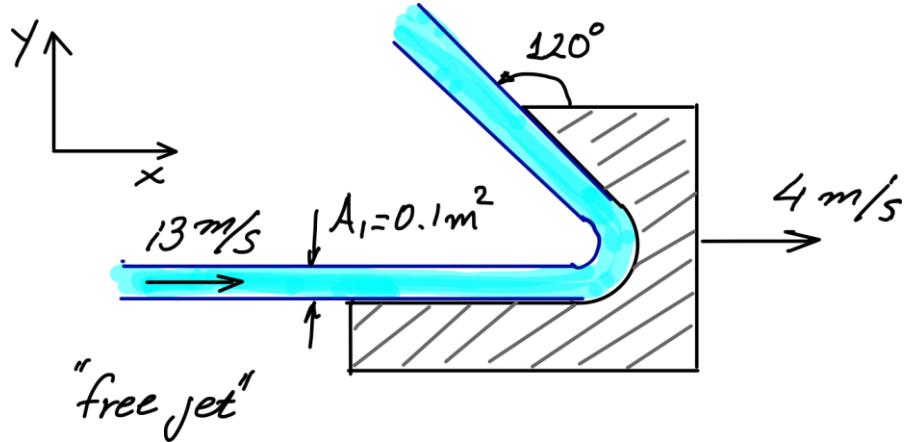
Froude number

$$\Rightarrow \left( \frac{h_2}{h_1} \right)^2 + \frac{h_2}{h_1} - 2 F_r^2 = 0$$

$$\Rightarrow \frac{h_2}{h_1} = \frac{-1 \pm \sqrt{1 + 8 F_r^2}}{2} \quad (\text{keep + sign})$$

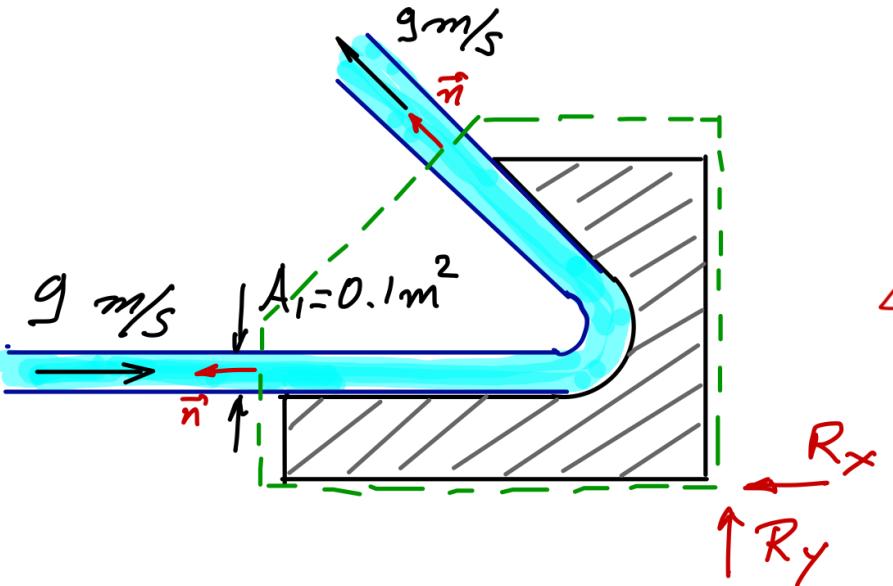
$$\Rightarrow \frac{h_2}{h_1} = \frac{1}{2} \left[ \sqrt{1 + 8 F_r^2} - 1 \right]$$

# Example: force on a moving vane



What is the force that the water jet exerts on the vane?

For an observer on the moving vane, the situation looks as follows:



"Free jet"

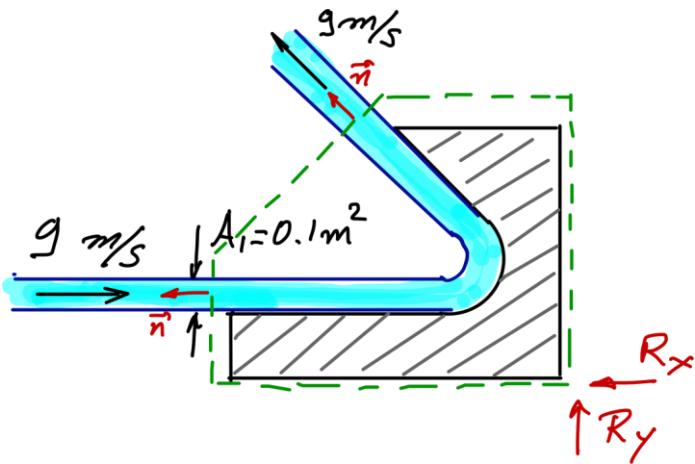
$\rightarrow P$  is  $\emptyset$  (atmospheric) everywhere in the jet

$$\cancel{P_1} + \frac{1}{2} \rho v_1^2 + \gamma z_1 = \cancel{P_2} + \frac{1}{2} \rho v_2^2 + \gamma z_2$$

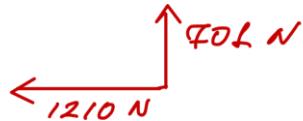
$$\Rightarrow v_1 = v_2 = 9 \text{ m/s}$$

Continuity:  $\rho_1 A_1 v_1 = \rho_2 A_2 v_2 \quad (\rho_1 = \rho_2)$

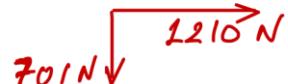
$$\Rightarrow A_2 = A_1 = 0.01 \text{ m}^2$$



The anchoring force to keep the vane in place:



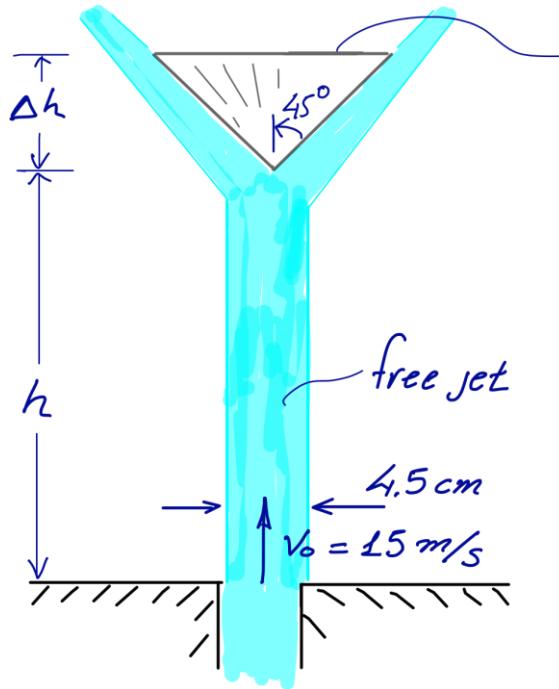
The force the water jet exerts on the vane:



$$\begin{aligned}
 x: \quad \int_{CS} u \rho \vec{v} \cdot \vec{n} dA &= \Sigma F_x \\
 V_1 \rho (-V_1) A_1 - V_2 \cos 60 \rho (V_2) A_2 &= -R_x \\
 \Rightarrow R_x &= \rho V_1^2 A_1 + \cos 60 \rho V_2^2 A_2 \\
 &= (1 + \cos 60) \rho V_1^2 A_1 \\
 &= 1.5 \times 999 \times 9^2 \times 0.1 \text{ N} \\
 &= \underline{1210 \text{ N}} \quad (\text{to the left})
 \end{aligned}$$

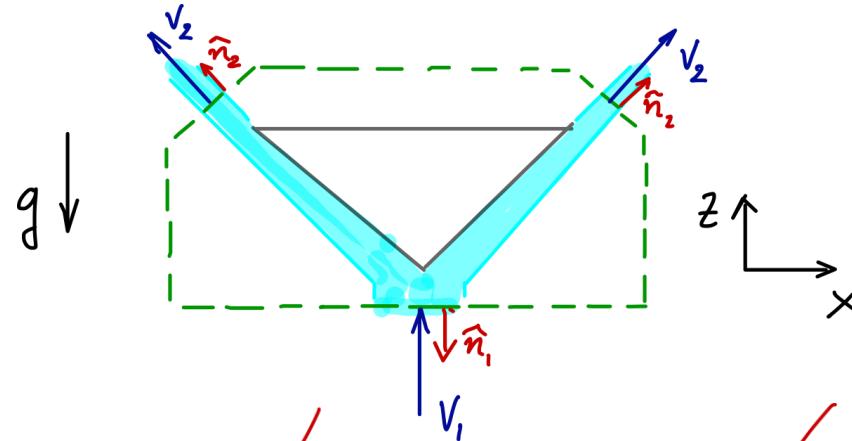
$$\begin{aligned}
 y: \quad \int_{CS} v \rho \vec{v} \cdot \vec{n} dA &= \Sigma F_y \\
 \Rightarrow V_2 \sin 60 \cdot \rho \cdot V_2 A_2 &= R_y \\
 \Rightarrow R_y &= \sin 60 \rho V_2^2 A_2 \\
 &= \sin 60 \cdot 999 \cdot 9^2 \cdot 0.01 \text{ N} \\
 &= \underline{701 \text{ N}} \quad (\text{up})
 \end{aligned}$$

# Cone suspended by a free water jet



$90^\circ$  cone  
weight,  $W_c = 50\text{ N}$

What is the suspension height,  $h$ ?  
Assume  $\Delta h \ll h$



Bernoulli:  ~~$P_1 + \frac{1}{2} \rho V_1^2 + \gamma z_1 = P_2 + \frac{1}{2} \rho V_2^2 + \gamma(z_2 + \Delta h)$~~

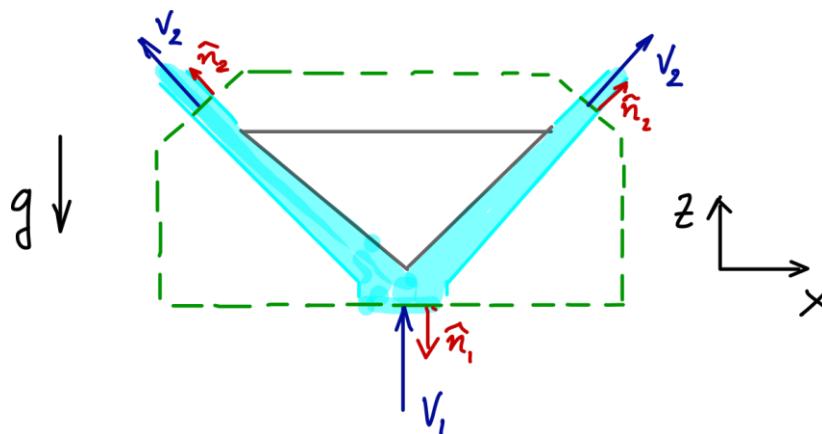
~~$\xrightarrow{O}$  free jet~~  ~~$\xrightarrow{O}$  free jet~~

$$\Rightarrow V_1 = V_2$$

Mass flux:  $\dot{m} = \rho V_0 A_0 = \rho V_1 A_1 = \rho V_2 A_2$

$$= 999 \frac{\text{kg}}{\text{m}^3} \cdot 15 \text{ m/s} \times \pi 0.0225^2 \text{ m}^2$$

$$= \underline{\underline{23.8 \text{ kg/s}}}$$



Momentum in z:  $\int_{CS} w \rho \vec{v} \cdot \vec{n} dA = \sum F_z$

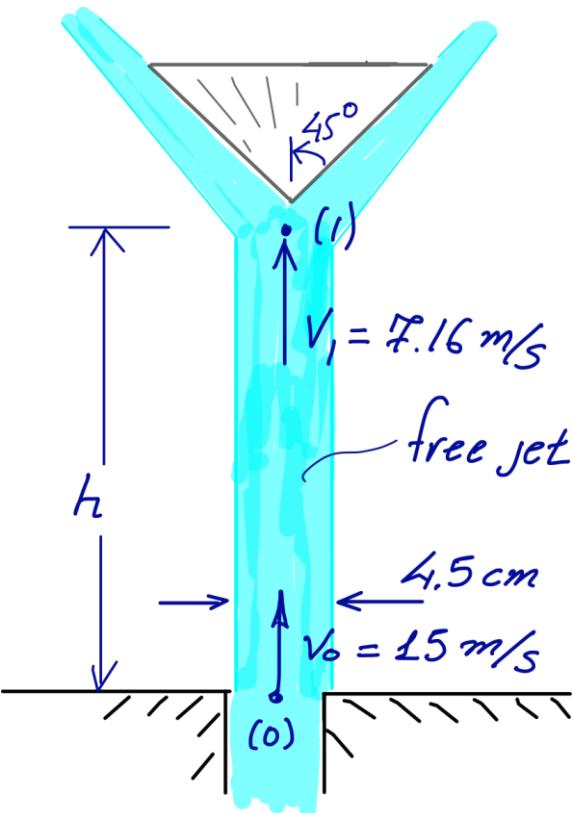
$$\Rightarrow v_1 \rho (-v_1) A_1 + (v_2 \cos 45) \cdot \rho \cdot v_2 A_2 = -W_c - \cancel{W_o}$$

$$\Rightarrow -v_1 (\underbrace{\rho v_1 A_1}_m) + v_2 \cos 45 (\underbrace{\rho v_2 A_2}_m) = -W_c$$

$$\Rightarrow m (-v_1 + v_2 \cos 45) = -W_c \quad (v_1 = v_2)$$

$$\Rightarrow m (1 - \cos 45) v_1 = W_c$$

$$\Rightarrow v_1 = \frac{W_c}{m (1 - \cos 45)} = \frac{50 \text{ N}}{23.8 \frac{\text{kg}}{\text{s}} \cdot (1 - \cos 45)} = \underline{\underline{7.16 \frac{\text{m}}{\text{s}}}}$$



Apply Bernoulli between (0) and (1)

$$\cancel{P}_0 + \frac{1}{2} \rho V_0^2 + \gamma z_0 = \cancel{P}_1 + \frac{1}{2} \rho V_1^2 + \gamma z_1$$

$$\Rightarrow \frac{1}{2} \rho (V_0^2 - V_1^2) = \gamma (z_1 - z_0) = \gamma h = \rho g h$$

$$\Rightarrow h = \frac{V_0^2 - V_1^2}{2g} = \frac{15^2 - 7.16^2}{2 \times 9.81} \text{ m}$$

$$\Rightarrow \underline{\underline{h = 8.85 \text{ m}}}$$